# The Crystal Structure of Ru<sub>4</sub>Al<sub>13</sub>

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The crystal structure of  $\mathrm{Ru_4Al_{13}}$  has been determined and refined by least-squares techniques on the basis of three-dimensional X-ray single-crystal data. The lattice parameters for the monoclinic cell are:

 $a = 15.86 \text{ Å}, b = 8.188 \text{ Å}, c = 12.74 \text{ Å}, \beta = 107.8^{\circ}$ 

The phase is isotypic with  ${\rm Fe_4Al_{13}}$ , space group C2/m. The relations between  ${\rm Os_4Al_{13}}$  and the  ${\rm Fe_4Al_{13}}$ -type of structure are discussed.

In previous reports on the crystal chemistry of aluminium alloys of the group VIII metals, the structures of some phases with the composition Me<sub>4</sub>Al<sub>13</sub> have been described viz. FeAl<sub>3</sub> (of ideal composition Fe<sub>4</sub>Al<sub>13</sub>)<sup>1,2</sup> Co<sub>4</sub>Al<sub>13</sub><sup>3</sup> and Os<sub>4</sub>Al<sub>13</sub>. The structures of Fe<sub>4</sub>Al<sub>13</sub> and Co<sub>4</sub>Al<sub>13</sub> are almost identical but differ considerably from that of Os<sub>4</sub>Al<sub>13</sub>. The compound Ru<sub>4</sub>Al<sub>13</sub> described in this work is isomorphous with Fe<sub>4</sub>Al<sub>13</sub>.

## **EXPERIMENTAL**

An alloy of the composition  $\mathrm{Ru_4Al_{13}}$  was prepared from ruthenium powder (L. Light & Co., about 99.99 %) and aluminium ribbon (E. Merck AG, at least 99.99 %) by melting in an electric arc furnace under an atmosphere of argon. The melt formed by the alloy is very brittle and crystalline. The crystals are prismatic and almost always twinned like those found in the corresponding  $\mathrm{Fe_4Al_{13}}$  compound. A single crystal could, however, be found and this was used to collect complete X-ray single-crystal data with  $\mathrm{Cu}K\alpha$  radiation. The Weissenberg photographs which were taken with [001] as the rotation axis showed monoclinic symmetry. About a thousand independent reflections from eight layer lines were estimated visually with a standard scale. The crystal was less than 0.01 mm in all dimensions and no correction for absorption was applied. The refinement of the structure was made by using a least-squares program on the computor FACIT EDB.

## THE REFINEMENT OF THE STRUCTURE

The structural similarity between the present phase and Fe<sub>4</sub>Al<sub>13</sub> was obvious from the X-ray data. Guinier powder photographs, registered with

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Number of Number of  $|F_{
m o}|$  $\sin \Theta$  $w \Delta^2$ independent  $w \Delta^2$ independent interval interval reflections reflections 0.00 - 0.460.88 180 0 - 451.16 181 45 - 90 90 - 135 135 - 180 180 - 225139 183 0.46 - 0.580.78 0.98 0.58 - 0.66 0.66 - 0.73 0.73 - 0.791.36 228 0.67 119 1.45 112 0.76 140 88 0.9398 1.18 225 - 270 270 - 315 0.79 - 0.841.04 98 0.72 56 0.84 - 0.880.8073 0.4932  $315 - 360 \\ 360 - 405$ 0.88 - 0.921.11 77 0.33 21 0.92 - 0.96 0.96 - 0.990.76 46 15 0.591.70 51 405 < 0.51 33

Table 1. Weight analysis in Ru<sub>4</sub>Al<sub>13</sub>.

 $\operatorname{Cu} K \alpha_1$  radiation and using KCl as an internal standard, gave the following cell dimensions in Å

$$a = 15.862 \pm 0.006$$
  
 $b = 8.188 \pm 0.003$   
 $c = 12.736 \pm 0.004$   $\beta = 107.77^{\circ} \pm 0.08$ 

These dimensions are similar to those reported for  $\mathrm{Fe_4Al_{13}}$  and  $\mathrm{Co_4Al_{13}}$ .  $\mathrm{Fe_4Al_{13}}$  has been described by Black  $^{1,2}$  as having the symmetry C2/m. The structure of  $\mathrm{Co_4Al_{13}}$  described by Hudd and Taylor  $^3$  is very similar to

Table 2. Final atomic parameters and their e.s.d.'s.

| Atom                    | <i>x</i>      | $\sigma(x)$ | y       | σ (y)  | z             | σ (z)  | B Å2 | $\sigma(B)$ Å <sup>2</sup> |
|-------------------------|---------------|-------------|---------|--------|---------------|--------|------|----------------------------|
| $Ru_1$                  | 0.0857        | 0.0002      | 0       |        | 0.3827        | 0.0003 | 0.41 | 0.04                       |
| $Ru_2$                  | 0.4017        | 0.0002      | 0       |        | 0.6233        | 0.0003 | 0.52 | 0.04                       |
| Ru <sub>3</sub>         | 0.0920        | 0.0002      | 0       |        | 0.9885        | 0.0003 | 0.51 | 0.04                       |
| $Ru_{m{\imath}}$        | 0.4007        | 0.0002      | 0       |        | 0.9853        | 0.0003 | 0.56 | 0.04                       |
| $Ru_{\kappa}$           | 0.3193        | 0.0001      | 0.2961  | 0.0002 | 0.2781        | 0.0002 | 0.57 | 0.03                       |
| $Al_6$                  | 0.0667        | 0.0007      | 0       |        | 0.1740        | 0.0012 | 1.05 | 0.18                       |
| Al,                     | 0.3208        | 0.0007      | 0       |        | 0.2812        | 0.0013 | 1.13 | 0.18                       |
| $Al_8$                  | 0.2383        | 0.0007      | 0       |        | 0.5354        | 0.0013 | 1.30 | 0.19                       |
| $\mathbf{Al}_{9}$       | 0.0724        | 0.0006      | 0       |        | 0.5805        | 0.0012 | 0.79 | 0.17                       |
| $\mathbf{Al}_{10}$      | 0.2396        | 0.0007      | 0       |        | 0.9565        | 0.0013 | 1.43 | 0.20                       |
| $Al_{11}^{10}$          | 0.4805        | 0.0006      | 0       |        | 0.8277        | 0.0011 | 0.55 | 0.15                       |
| $Al_{12}$               | $\frac{1}{2}$ |             | 0       |        | $\frac{1}{2}$ |        | 1.09 | 0.25                       |
| $Al_{13}$               | 0.3112        | 0.0006      | 0       |        | 0.7729        | 0.0011 | 0.53 | 0.15                       |
| $\mathbf{Al}_{14}$      | 0.0834        | 0.0007      | 0       |        | 0.7874        | 0.0013 | 1.33 | 0.19                       |
| $\mathbf{Al}_{15}$      | 0.1859        | 0.0005      | 0.2197  | 0.0009 | 0.1098        | 0.0009 | 0.99 | 0.12                       |
| $Al_{16}$               | 0.3657        | 0.0004      | 0.2168  | 0.0008 | 0.1107        | 0.0008 | 0.81 | 0.12                       |
| Al,                     | 0.1770        | 0.0005      | 0.2222  | 0.0010 | 0.3342        | 0.0009 | 1.41 | 0.13                       |
| $\mathbf{Al}_{18}$      | 0.4909        | 0.0005      | *0.2332 | 0.0009 | 0.3298        | 0.0009 | 1.00 | 0.12                       |
| $Al_{19}^{10}$          | 0.3639        | 0.0004      | 0.2256  | 0.0009 | 0.4822        | 0.0008 | 0.88 | 0.12                       |
| $\mathbf{Al}_{20}^{10}$ | 0             |             | 0.2499  | 0.0012 | 0             |        | 0.69 | 0.16                       |

<sup>\*</sup> corresponding coordinate given by Black is probably a misprint.

Table 3. Part of the Guinier powder pattern of  $Ru_4Al_{13}$  ( $CuK\alpha_1$ ).

|   |                                 |                                | * 10 (                       | •             |
|---|---------------------------------|--------------------------------|------------------------------|---------------|
| h k l   | $10^5 \sin^2 m{	heta}_{ m obs}$ | $10^5 \sin^2 \Theta_{ m calc}$ | $I_{ m obs}$                 | $I_{ m calc}$ |
| 0 0 1   |                                 | 403                            |                              | 0.3           |
|   | _                               | 1040                           |                              | 0.4           |
| $\overline{2}$ 0 1  |                                 | 1048                           | _                            | 0.0           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 1144                            | 1145                           | $\mathbf{v}\mathbf{w}$       | 2.8           |
| Ī 1 1   | 1 <b>34</b> 8                   | 1350                           | w                            | 13.7          |
| 002   |                                 | 1613                           |                              | 1.3           |
|   | 1747                            | 1746                           | $\mathbf{w}$                 | 8.8           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 1839                            | 1839                           | vvw                          | 1.8           |
| $\overline{2}$ 0 2  | 1859                            | 1863                           | $\mathbf{v}\mathbf{w}$       | 2.4           |
| 1 1 2   | _                               | 2363                           |                              | 0.1           |
| 3 1 1   |                                 | 3035                           |                              | 0.0           |
| 1 1 2   | _                               | 3154                           | _                            | 0.5           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | _                               | 3225                           |                              | 0.2           |
| 2 0 2   | 3442                            | 3444                           | $\mathbf{st}$                | 51.1          |
| $\overline{2}$ 0 3  | 3482                            | 3484                           | $\mathbf{st}$                | 56.2          |
| 0 2 0   | 3438                            | 3540                           | m                            | 19.2          |
| 0 0 3   | 3626                            | <b>363</b> 0                   | $\mathbf{st}$                | 79.8          |
| $\begin{array}{cccc} 0 & 0 & 3 \\ \overline{3} & 1 & 2 \\ \overline{4} & 0 & 1 \end{array}$ | _                               | 3652                           |                              | 0.2           |
|   | 3773                            | 3773                           | m                            | 20.2          |
| 0 2 1   | <b>3946</b>                     | 3943                           | vw                           | 5.8           |
| 4 0 0   | 4164                            | 4160                           | ${f st}$                     | 43.9          |
| 1 1 3   | -                               | 4181                           |                              | 0.1           |
| <b>4</b> 0 2  | 4194                            | 4192                           | $\operatorname{\mathbf{st}}$ | 41.9          |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |                                 | 4221                           | _                            | 0.2           |
| 2 2 0   | $\sim 4582$                     | <b>∫4580</b>                   | $\mathbf{vst}$               | <b>∫</b> 56.5 |
| $\bar{2} \ 2 \ 1$   |                                 | <b>\4588</b>                   |                              | (42.5         |
|   |                                 | 5076                           |                              | 0.0           |
| 0 2 2   | 5154                            | 5153                           | st                           | 62.8          |
| 4 0 1   |                                 | (5354)                         |                              | $\{19.8$      |
| 1 1 3   |                                 | 5368                           |                              | 0.6           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\sim 5380$                     | {5378                          | $\mathbf{vst}$               | 35.4          |
| $\overline{2}$ 2 2  |                                 | 5402                           |                              | 26.9          |
| <b>4</b> 0 3  |                                 | 15418                          |                              | 51.2          |
| $\begin{array}{cccc} 2 & 0 & 3 \\ \overline{2} & 0 & 4 \end{array}$                         | 5854                            | 5856                           | vw                           | 8.9           |
| $\bar{2}$ 0 4   | $\bf 5912$                      | 5912                           | vw                           | 10.8          |
| 3 1 2   |                                 | 6025                           | _                            | 0.4           |
| 004   | <b>6458</b>                     | 6453                           | vw                           | 4.5           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |                                 | 6800                           |                              | 0.0           |
| Ī 1 4   | _                               | 6807                           | _                            | 0.4           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 6982                            | 6984                           | vw                           | 4.4           |
| $\frac{1}{5}$ $\frac{1}{2}$   |                                 | 7022                           |                              | 0.0           |
|   | 7026                            | 7024                           | vw                           | 3.3           |
| 0 2 3   | 1775                            | 7170                           | vw                           | 6.9           |

 ${\rm Fe_4Al_{13}}$  but was found to have the lower space group Cm. The latter symmetry permits the separation of 8- and 4-fold positions of C2/m into two sets of 4- and 2-fold positions respectively.

The investigation of  $\mathrm{Ru_4Al_{13}}$  was started using the structure reported for  $\mathrm{Fe_4Al_{13}}$  as a trial model. The structure was refined by the least-squares method. The weights were calculated using Hughes' weighting scheme. The final R value was 0.114. The weight analysis obtained in the last cycle of refinement is given in Table 1, the final atomic parameters in Table 2 and the Guinier pattern in Table 3.

Table 4. The interatomic distances in  $\mathrm{Ru_4Al_{13}}$ . Upper limit 3.3 Å. The numbers represent: central atom, neighbour (number of such neighbours), followed by the distance in Å.

| 1 - 6(1) 2.582     | 6-1(1) 2.582   | 12 - 2(2) 2.528           | 17 1(1) 2.517  |
|--------------------|--|---------------------------|----------------|
| 8(1) 2 602         | 3(1) 2 514   | 18(4) 2.859               | 2(1) 2 727     |
| 0(1) 9 501         | 2(1) 9 707   | 10(4) 9.700               | 5/1\ 9.620     |
| 9(1) 2.591         | 3(1) 2.727   | 19(4) 2.790               | 0(1) 2.000     |
| 9(1) 2.687         | 14(1) 2.573  |                           | 6(1) 2.891     |
| 14(1) 2.887        | 15(2) 2.902  | 13-2(1) 2.712             | 7(1) 3.148     |
| 17(2) 2.517        | 17(2) 2.891  | 4(1) 2.644                | 8(1) 3.049     |
| 18(2) 2.621        | 20(2) 2.964  | 5(2) 2.583                | 8(1) 2.894     |
| 10(2) 2.705        | 20(2) 2:001  | 8/1\ 2.800                | 12/1\ 2.692    |
| 10(2) 2.100        | 7 5/0\ 0.405   | 10(1) 9.005               | 15(1) 2.000    |
| 0 0/11 0 400       | I - 3(2) 2.423   | 10(1) 2.899               | 10(1) 2.904    |
| 2-8(1) 2.490       | 15(2) 3.119  | 11(1) 2.559               | 18(1) 2.957    |
| 11(1) 2.520        | $16(2) \ \ 3.053$  | 15(2) 2.731               | 19(1) 2.988    |
| 12(1) 2.528        | 17(2) 3.148  | 17(2) 2.688               | 19(1) 2.645    |
| 13(1) 2.712        | 18(2) 3.208  | - ( )                     |                |
| 17(9) 9 797        | 19/2) 3.060  | 14 - 1/1\ 9.997           | 19 1/1\ 9.691  |
| 10(0) 0 507        | 13(2) 3.000  | 2(1) 0 500                | 0(1) 0 507     |
| 18(2) 2.507        | 0 1/11 0 000   | 3(1) 2.522                | 2(1) 2.507     |
| 19(2) 2.519        | 8- 1(1) 2.602  | 5(2) 2.579                | 5(1) 2.649     |
|                    | 2(1) 2.489   | 6(1) 2.573                | 7(1) 3.208     |
| $3 - 3(1) \ 3.022$ | 5(2) 3.255   | 9(1) 2.588                | 9(1) 2.791     |
| 6(1) 2.514         | 9(1) 2.860   | 10(1) 2.742               | 11(1) 2.903    |
| 6(1) 9 797         | 12/1\ 2.000  | 16(2) 2.712               | 19/1\ 9.850    |
| 10(1) 2.727        | 15(1) 2.050  | 10(2) 2.000               | 14(1) 9.705    |
| 10(1) 2.495        | 17(2) 3.049  | 18(2) 2.705               | 14(1) 2.705    |
| 14(1) 2.522        | 17(2) 2.894  |                           | 16(1) 2.892    |
| 15(2) 2.538        | 19(2) 2.943  | 15 - 3(1) 2.538           | 17(1) 2.957    |
| 16(2) 2.817        | 19(2) 2.739  | 4(1) 2.758                | 19(1) 3.197    |
| 20(2) 2 543        | ()   | 5(1) 2.586                | 19(1) 2 771    |
| 20(2) 2.010        | 0 1/1\ 9.501   | 6/1) 2.000                | 10(1) 21       |
| 4 4/3) 9.056       | 9-1(1) 2.091   | 0(1) 2.902                | 10 1/1) 0 505  |
| 4-4(1) 3.056       | 1(1) 2.087   | 7(1) 3.119                | 19- 1(1) 2.795 |
| 10(1) 2.469        | 5(2) 2.664   | 10(1) 2.965               | 2(1) 2.519     |
| 11(1) 2.679        | 8(1) 2.860   | 10(1) 2.826               | 5(1) 2.543     |
| 11(1) 2.547        | 9(1) 2.569   | 13(1) 2.731               | 7(1) 3.060     |
| 13(1) 2.644        | 14(1) 2.588  | 16(1) 2.848               | 8(1) 2.943     |
| 15/9) 9 759        | 19/9) 9 701  | 16(1) 9 795               | 9/1\ 9.730     |
| 10(2) 2.700        | 10(2) 2.701  | 10(1) 2.720               | 0(1) 2.100     |
| 10(2) 2.500        | 19(2) 2.083  | 17(1) 2.904               | 9(1) 2.000     |
| 20(2) 2.555        |  | 20(1) 2.863               | 12(1) 2.798    |
|                    | 10-3(1) 2.495  |                           | 17(1) 2.988    |
| 5-7(1) 2.425       | 4(1) 2.468   | 16 - 3(1) 2.817           | 17(1) 2.645    |
| 8(1) 3.255         | 5(2) 3.298   | 4(1) 2.560                | 18(1) 3.120    |
| 9(1) 2 664         | 13(1) 2.805  | 5(1) 2.543                | 18/1\ 2.771    |
| 10(1) 2.004        | 14(1) 9740   | 7/1\ 9 059                | 10(1) 2.771    |
| 10(1) 0.298        | 14(1) 2.742<br>17(0) 0.007   | /(1) 0.000<br>10/1) 0.007 | 00 4(0) 0 744  |
| 13(1) 2.583        | 15(2) 2.965  | 10(1) 2.935               | 20-4(2) 2.544  |
| 14(1) 2.579        | 15(2) 2.828  | 10(1) 2.833               | 5(2) 2.555     |
| 15(1) 2.586        | 16(2) 2.935  | 11(1) 2.925               | 7(2) 2.963     |
| 16(1) 2.543        | 16(2) 2.833  | 14(1) 2.659               | 11(2) 2.948    |
| 17(1) 2.638        | (-, -:::3  | 15(1) 2.848               | 15(2) 2 863    |
| 18(1) 2.840        | 11_ 9/1) 9 590   | 15/1\ 9.795               | 16/9\ 9 004    |
| 10(1) 4.048        | 4/1\ 0.02U   | 10(1) 2.720               | 10(2) 2.504    |
| 19(1) 2.043        | 4(1) 2.079   | 18(1) 2.892               |                |
|                    | 4(1) 2.547   | 20(1) 2.904               |                |
|                    | 13(1) 2.559  |                           |                |
|                    | 16(2) 2.925  |                           |                |
|                    | 18(2) 2.903  |                           |                |
|                    | 6-1(1) 2.582 3(1) 2.514 3(1) 2.727 14(1) 2.573 15(2) 2.902 17(2) 2.891 20(2) 2.964  7-5(2) 2.425 15(2) 3.119 16(2) 3.053 17(2) 3.148 18(2) 3.208 19(2) 3.060  8-1(1) 2.602 2(1) 2.489 5(2) 3.255 9(1) 2.860 13(1) 2.860 13(1) 2.890 17(2) 3.049 17(2) 2.894 19(2) 2.943 19(2) 2.739  9-1(1) 2.591 1(1) 2.687 5(2) 2.664 8(1) 2.860 9(1) 2.569 14(1) 2.588 18(2) 2.791 19(2) 2.683  10-3(1) 2.495 4(1) 2.468 5(2) 3.298 13(1) 2.895 14(1) 2.742 15(2) 2.965 15(2) 2.828 16(2) 2.935 16(2) 2.833  11-2(1) 2.520 4(1) 2.547 13(1) 2.559 16(2) 2.925 18(2) 2.903 20(2) 2.948 |                           |                |
|                    | 20(2) 2.010  |                           |                |
|                    |  |                           |                |

| Compound                          | Bond                        | CN     | Range of distance in Å | Average<br>distance in Å |
|-----------------------------------|-----------------------------|--------|------------------------|--------------------------|
| Al fee                            | Al-Al                       | 12     |                        | 2.86                     |
| Fe bcc 20°C                       | $\mathbf{Fe} - \mathbf{Fe}$ | 8      |                        | 2.48                     |
| Fe fcc 916°C                      | $\mathbf{Fe} - \mathbf{Fe}$ | 12     |                        | $\frac{2.57}{2.57}$      |
| Ru hep                            | Ru-Ru                       | -6 + 6 | 2.65 - 2.71            | 2.68                     |
| Os hep                            | Os - Os                     | 6+6    | 2.68 - 2.74            | 2.71                     |
| $\mathbf{Fe}_{4}\mathbf{Al}_{13}$ | $\mathbf{Fe} - \mathbf{Al}$ | ~10    | 2.26 - 2.84            | 2.55                     |
| 13                                | Al-Al                       |        | 2.45-                  |                          |
| $Ru_{4}Al_{13}$                   | Ru-Al                       | ~10    | 2.43 - 2.89            | 2.60                     |
|                                   | Al-Al                       |        | 2.56-                  |                          |
| $Os_4Al_{13}$                     | Os-Al                       | 10, 11 | 2.46 - 2.86            | 2.65                     |
| 419                               | Al—Al                       | ~10    | 2.57 - 2.96            | 2.79                     |

Table 5. Distances in Me<sub>4</sub>Al<sub>13</sub> compounds and their elements.

The non-centrosymmetric  $\text{Co}_4\text{Al}_{13}$  was then taken as a trial structure in a second calculation but the result showed no indications of  $\text{Ru}_4\text{Al}_{13}$  having a lower symmetry than C2/m.

Several aluminium sites of  $\text{Fe}_4\text{Al}_{13}$  and  $\text{Co}_4\text{Al}_{13}$  are reported to be partially occupied by 30—70 % aluminium. According to the B values given in Table 2 there seems to be no such extensive partial occupation by aluminium in  $\text{Ru}_4\text{Al}_{13}$ .

## DISCUSSION

The interatomic distances are given in Table 4. The standard deviations for these are less than 0.02 Å. The numbering of the atoms in this table and in Table 2 is the same as used by Black in the first paper on Fe<sub>4</sub>Al<sub>13</sub>. In the second paper on Fe<sub>4</sub>Al<sub>13</sub>, where the interatomic distances are given, the atoms Al<sub>7</sub> and Al<sub>14</sub> have been interchanged.

A comparison between the atomic distances of Fe<sub>4</sub>Al<sub>13</sub> and Ru<sub>4</sub>Al<sub>13</sub> shows that the coordinations around equivalent atoms in the two structures are the same. However, the ranges of distance are different as shown in Table 5. This is because of the extremely short distances found in Fe<sub>4</sub>Al<sub>13</sub>. On the other hand, the ranges of distance found in Ru<sub>4</sub>Al<sub>13</sub> are almost identical to those found in Os<sub>4</sub>Al<sub>13</sub>, except for the upper limit of the Al—Al distances (cf. Table 5). According to the distribution of Al—Al distances around 3 Å found in Ru<sub>4</sub>Al<sub>13</sub> there is no definite upper limit like that found for Al—Al distances in Os<sub>4</sub>Al<sub>13</sub>. Well defined coordination shells indicating close packing are formed around all the atoms of Os<sub>4</sub>Al<sub>13</sub> and all the ruthenium atoms of Ru<sub>4</sub>Al<sub>13</sub>. This is not the case with all the aluminium atoms of Ru<sub>4</sub>Al<sub>13</sub> and is caused by the aluminium atom numbered 7 which has only two contacts closer than 3.0 Å.

The average distances in the elements are given in Table 5. Os and Ru have about the same size and are considerably larger than Fe. According to this and the fact that  $Os_4Al_{13}$  is better packed,  $Ru_4Al_{13}$  should have the  $Os_4Al_{13}$  structure from geometrical reasons. This is, however, not the case and the  $Ru_5$  atom seems to play an important role in this connection. The arrangement around  $Ru_1-Ru_4$  is very similar to the arrangement around the Os atoms

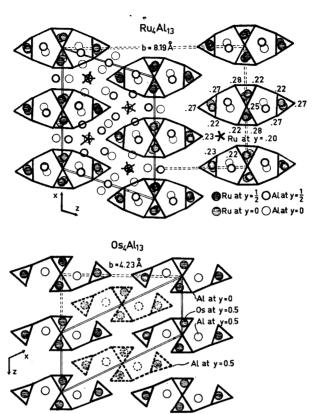


Fig. 1. The atomic arrangements in  $Os_4Al_{13}$  and  $Ru_4Al_{13}$ . There is an aluminium atom at each corner of the triangles. These aluminium atoms form a puckered net at around y=1/4 in  $Ru_4Al_{13}$ . The deviation from planarity is indicated in one of the figures of  $Ru_4Al_{13}$ . The cell dimensions for  $Os_4Al_{13}$  are: a=17.64 Å, b=4.228 Å, c=7.773 Å,  $\beta=115.15^\circ$ .

in  $Os_4Al_{13}$  but differs completely from that around  $Ru_5$ . This fact is illustrated in Fig. 1.  $Os_4Al_{13}$  may be described as built up from column-like arrangements of the composition  $Os_4Al_{13}$  the projections of which are indicated in the figure. Very similar units of the same composition and containing  $Ru_1-Ru_4$  are found in the ruthenium phase. The  $Ru_5$  atoms, at the asterisk-like positions in the figure, form almost straight  $Ru_5-Al_7-Ru_5$  bonds along [010] and force  $Al_7$  to have no other contact closer than 3.0 Å.

No explanation why the composition is the same in the two compounds has been found.

When looking at a three-dimensional model of Ru<sub>4</sub>Al<sub>13</sub> the most striking feature is the regular arrangement of the Ru atoms. Ru<sub>5</sub> is in the centre of a deformed petagonal prism formed by the other ruthenium atoms. Only fragments of this pattern are found in Os<sub>4</sub>Al<sub>13</sub>.

Compounds of similar composition and structures seem to exist in the rhodium and palladium systems. The crystals of these form very complicated twins but give a zero layer Weissenberg photograph around a rotation axis of 16.6 Å, which, as far as the strong reflections are concerned, is very like the corresponding zero layer photograph of Ru<sub>4</sub>Al<sub>13</sub>. The strong spots are approximately arranged in a 5-fold symmetry but this is more exactly so in the Pd and Rh compounds and these have much larger unit cells.

It seems likely that the approximately five-fold symmetry observed in the single-crystal patterns of these new, very complicated phases reflects an even more regular transition-metal structure than that found in Ru<sub>4</sub>Al<sub>13</sub>.

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